

# **480 μA, 6.5MHz, RRIO CMOS Operational Amplifier**

## **Description**

- SL8631 (single-channel), SL8632 (dual-channel), and SL8634 (quad-channel) are operational amplifiers designed for low noise, low voltage, and low power applications. The SL863x series features a bandwidth of 6.5MHz, a slew rate of 4V/μs, and a static current of 480μA per amplifier (at a 5V supplyvoltage). They are suitable for various applications.
- The SL863x operational amplifiers are widely used in low-voltage and low-noise systems to provide optimal performance. Their input common-mode voltage range includes ground, with a maximum input offset voltage of 4.2mV.SL863x amplifiers can drive rail-to-rail output swings under heavy output loads.
- The SL863x series operates with single supplies from +2.1V to +5.5V or dual supplies. All models are specified to operate within an extended industrial temperature range of -40°C to +125°C.
- SL8631 is available in 5-pin SC70 and SOT-23 packages. SL8632 is offered in 8-pin MSOP, DFN2\*2, TSSOP, and SOP packages. SL8634 is packaged in 14-pin TSSOP and SOP configurations.

## **Feature**

- High Slew Rate: 4V/µs
- Gain-Bandwidth Product: 6.5MHz
- Low Power Consumption: 480μA per amplifier
- 0.1% Settling Time (for a 2V step): 1μs
- Low Noise: 20nV/√Hz@10kHz
- $\bullet$  High Gain: 103dB
- Low Offset Voltage: 4.2mV (maximum)
- **•** Unity Gain Stable
- Rail-to-Rail Input and Output ----- Input Voltage Range: -0.1V to +5.1V (at 5V supply voltage)
- Operating Supply Range: +2.1V to +5.5V
- Operating Temperature Range: -40°C to +125°C

## **Application**

- Photodiode and sensor interfaces
- Audio output
- Active filters
- Driving A/D converters
- Portable devices and battery-powered equipment



# **Pin configuration**



## **Pin function**





# **Ordering information**





# **Absolute maximum rating** (TA=25℃)



Note:

1. Exceeding the absolute maximum ratings may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions beyond those indicated under recommended operating conditions is not implied. Prolonged exposure to absolute maximum ratings conditions may affect device reliability.

2. Input terminals are clamped to the power supply rails with diodes.

3. The provided device will never exceed the maximum junction temperature  $(T<sub>J</sub>)$  at any time.



## **Electrical Parameter**





## **Electrical Parameter**







### **Typical characteristics curves**

(T<sub>A</sub>=+25℃, V<sub>cM</sub>=V<sub>s</sub>/2, RL=10kΩ connect to V<sub>s</sub>/2, Unless otherwise specified )



Input offset voltage distributio



Power supply rejection ratio and<br>common mode rejection ratio versus frequency





Relationship between input bias current and temperature



Open-loop gain and phase margin versus frequency



Large signal step response at 2.7V Small signal step response at 2.7V



## **Typical characteristics curves**

( $T_A$  = +25°C,  $V_{CM}$  =  $V_S/2$ ,  $R_L$  = 10k $\Omega$  connect to  $V_S/2$ , Unless otherwise specified)



Large signal step response at 5V Small signal step response at 5V



## **Application**

### **1. Low input bias current**

The SL863x is a series of CMOS operational amplifiers known for their extremely low input bias currents in the pA range. The low input bias current allows the amplifier to be used in applications with high-resistance sources, but care must be taken to minimize PCB surface leakage currents. For more details, please refer to the "PCB Surface Leakage" section below.

### **2. PCB Surface Leakage**

In applications that demand low input bias currents, consideration must be given to the phenomenon of surface leakage on printed circuit boards (PCB). Surface leakage is caused by moisture, dust, or other contaminants present on the PCB. Under low humidity conditions, the typical resistance between adjacent traces can be as high as 10^12 ohms. A voltage difference of 5V between them can result in a current flow of 5pA, which exceeds the input bias current of the SL863x operational amplifier at +25℃ (typical value  $\pm$ 1pA).

It is recommended to employ a multilayer PCB layout and route the –IN and +IN signals of the operational amplifier beneath the PCB surface to mitigate surface leakage effects.

An effective method to reduce surface leakage is to use guard rings around sensitive pins (or traces). These guard rings are biased at the same voltage as the sensitive pins. Such a layout example for an inverting gain application is illustrated in Figure 10.

1. For non-inverting gain and unity gain buffers:

a) Use wires that do not contact the PCB surface to connect the non-inverting input pin (+IN) to the input. b) Connect a guard ring to the inverting input pin (-IN). This biases the guard ring to the common-mode input voltage.

2. For inverting gain and transimpedance amplifiers (converting current to voltage, e.g., for photodetectors): a) Connect a guard ring to the non-inverting input pin (+IN). This biases the guard ring to the same reference voltage as the operational amplifier (e.g., VS/2 or ground).

b) Use wires that do not contact the PCB surface to connect the inverting input pin (-IN) to the input.



Using guard rings around sensitive pins.



### **3. Rail-to-Rail Feature**

The SL863x series has an input common-mode voltage range that can exceed the power supply rails by 300mV. This is achieved through a complementary input stage — a parallel combination of an N-type MOS input differential pair and a P-type MOS input differential pair. For normal operation, inputs should be limited within this range. The absolute maximum input voltage exceeds the power supply voltage by 500mV.

Inputs that are outside the input common-mode range but below the maximum input voltage are ineffective but do not cause any damage to the op-amp.Unlike some other operational amplifiers, if the input current is limited, the input may exceed the power supply without phase inversion, as shown in Figure 11. Due to the extended input common-mode range from (VS- - 0.1V) to (VS+ + 0.1V), the SL863x operational amplifier can achieve 'true ground' detection.



Phase free flipping when the input exceeds the power supply voltage

The AB class output stage topology of the common-source transistor can achieve rail-to-rail output. For light resistive loads (e.g., 100kΩ), the output voltage typically swings to within 5mV of the power supply rails. Under moderate resistive loads (e.g., 10kΩ), the output can swing to within 15mV of the power rails while maintaining high open-loop gain.The maximum output current depends on the total power supply voltage. As the amplifier's power supply voltage increases, so does its output current capability. When the output is continuously short-circuited, care must be taken to keep the IC junction temperature below 150°C.

The amplifier's output includes reverse-biased ESD diodes connected to each power supply. The output should not be forced beyond 0.5V of either power supply, as this would cause current to flow through these diodes.



### **4. Capacitive Load and Stability**

The SL863x can directly drive 1nF at unity gain without oscillation. Unity gain followers (buffers) are the circuits most sensitive to capacitive loads.

Directly driving capacitive loads can reduce the phase margin of the amplifier, leading to ringing or even oscillation. Applications requiring higher capacitive drive capability should use isolation resistors between the output and the capacitive load, as shown in Figure 12. The isolation resistor  $R_{\text{ISO}}$  and the load capacitor  $C_L$  form a zero to improve stability. A larger value of R<sub>ISO</sub> provides more stable V<sub>OUT</sub>. Note that this method causes gain accuracy loss because  $R_{ISO}$  forms a voltage divider with  $R_L$ .



Indirectly drive capacitive load

Improve the circuit as shown in Figure 13. It ensures DC precision while also maintaining AC stability.  $R_F$  provides DC precision by connecting the inverted signal to the output.

 $C_F$  and R<sub>ISO</sub> maintain phase margin throughout the feedback loop by feeding back high-frequency components of the output signal to the amplifier's inverting input, compensating for phase margin loss.



**Driving capacitive loads with DC precision indirectly.**

For circuits with non-unity gain, there are two additional methods to increase phase margin: (a) by increasing the amplifier gain, or (b) by paralleling capacitors with feedback resistors to cancel parasitic capacitance associated with the inverting node.



### **5. Power Supply Layout and Filtering**

The SL863x series operates with a single supply from +2.1V to +5.5V or dual supplies from ±1.05V to ±2.25V. For single-supply operation, filtering ceramic capacitors (0.01μF to 0.1μF) should be placed within 2mm of the VS pin to achieve good high-frequency performance.

In dual-supply operation, separate 0.1μF ceramic capacitors should be connected to ground for both VS+ and VS– power supplies. Larger capacitors (2.2μF or greater tantalum capacitors)within 100mm can provide large and slow current and improve overall performance. These larger capacitors can be shared with other analog devices.

Effective PCB layout techniques optimize performance by reducing stray capacitance at the inputs and outputs of operational amplifiers. To minimize stray capacitance, external components should be placed as close to the chip as possible, minimizing trace lengths and widths, and utilizing surface-mount devices wherever feasible.

For operational amplifiers, it is strongly recommended to solder devices directly onto the PCB to minimize loop area for high-frequency and high-current paths, thus reducing EMI (electromagnetic interference).

### **6. Grounding**

In SL863x circuit design, the ground plane is critical. The length of current paths in the ground return lines can generate unwanted voltage noise, and a wide ground area helps to reduce parasitic inductance.

### **7. Input-Output Coupling**

To minimize capacitive coupling, input and output signal traces should not be routed parallel to each other. This helps reduce undesired positive feedback.



## **Typical application circuit diagram**

#### **1. Differential Amplifie r**



Circuit shown in Figure 14 implements differential functionality. If the resistance ratio is  $R4/R3 = R2/R1$ , then:  $V_{\text{OUT}} = (V_{\text{p}} - V_{\text{n}}) \times R_{2}/R_{1} + V_{\text{REF}}$ 

### **2. Instrumentation Amplifier**



The SL863x series is well-suited for conveying sensor signals in battery-powered applications. Figure 15 illustrates an instrumentation amplifier using two operational amplifiers from the SL863x series. This circuit is suitable for applications requiring high gain to suppress common-mode noise. The reference voltage ( $V_{REF}$ ) is provided by a low impedance source. In single-supply voltage applications,  $V_{REF}$  is typically set to  $V_s/2$ .



## **Typical application circuit diagram**

### **3. Chemical Sensor**



All components contained within the probe

### Figure pH probe

The input bias current of the SL863x series is within the pA range, making it an ideal choice for buffering highimpedance chemical sensors such as pH probes. For instance, the circuit in Figure 16 eliminates the need for expensive low-leakage cables when connecting pH probes (like the universal combination pH probe, e.g., Corning 476540) to measurement ICs such as ADCs, AFEs, and/or MCUs.

An SL863x operational amplifier and a lithium battery are integrated into the probe assembly. Traditional low cost coaxial cables are used to transmit the output signal of the operational amplifier to subsequent ICs for pH value reading.

### **4.Current Sensing Amplifier Based on Shunt**

The slew rate of the current sensing amplifier output sinusoidal signal shown in Figure 17 is  $2\pi f_{VPP}$ , and the slew rate of the output triangular wave signal is 2fVPP. In most motor control systems, PWM frequencies range from 10kHz to 20kHz. For a PWM frequency of 10kHz, one period lasts 100μs. In motor current sensing, phase currents are converted to phase voltage signals for ADC sampling.

This sampling voltage signal must be established before entering the ADC. As shown in Figure 8, the total establishment time of the current shunt monitor circuit includes: the rise delay time  $(t_{SR})$  due to the slew rate of the operational amplifier, and the measurement establishment time  $(t<sub>SET</sub>)$ .

If the minimum duty cycle of PWM is defined as 5%, and t<sub>sR</sub> needs to perform phase current monitoring at 20% of the total time window, for a 3.3V motor control system (with a 12-bit ADC of 3.3V MCU), the slew rate of the operational amplifier should be greater than:

### 3.3V/(100μs×5%×20%)=3.3V/μs

Simultaneously, the bandwidth of the operational amplifier should be significantly greater than the PWM frequency (at least 10 times higher).



# <sup>T</sup>ypica<sup>l</sup> application circuit diagram



Figure current shunt monitoring circuit







# **SOT23-5**





# **SC70-5 (SOT353)**





## **MSOP-8**



## **SOP-8**











**DFN8-L 2\*2**

**TSSOP-8**











## **SOP-14**





# **TSSOP-14**